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OXIDATION OF NITINOL

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OXIDATION OF NITINOL

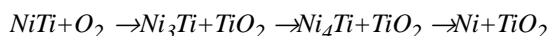
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ABSTRACT

This study explores the kinetics and phase transformations of oxide formation in NiTi. Electropolished Ni-50.8 at.%Ti wires were heat treated between 400 and 1000° C for 3 to 300 min. in air. Surface analytical techniques were used to characterize the thickness, composition, and phase distribution of the oxide surface layers. It was observed that the oxide growth is parabolic with resultant activation energy of 50 kcal/mol, which is comparable to the oxidation of pure Ni and Ti. The results of this study suggests that oxidation occurs as follows:



The presence, amount, and distribution of these phases depend on both time and temperature. The composition of the oxides and how it influences biocompatibility are discussed.

KEYWORDS

Nitinol, Oxidation, Heat Treatment, Kinetics, Phase Transformation, Corrosion

INTRODUCTION

A number of authors have discussed the unique material properties and biocompatibility that NiTi offers [1–5]. The nearly nickel-free TiO₂ layer of electropolished NiTi has been proven to be an excellent source of corrosion protection; however, the release of nickel ions during the degradation of NiTi is a significant concern when considering its use as an implant material [5–6]. At elevated temperatures in air, titanium reacts with oxygen to form a TiO₂ layer, and the structure of this oxide is important in understanding the biocompatibility of the material. Several authors [7–11] have studied the effects of surface treatments on the surface composition of NiTi, but the mechanisms of

high temperature oxidation and the effects on corrosion are not entirely understood. This study investigates the phenomena of oxide formation by means of various surface analytical techniques and includes the exploration of oxidation kinetics as well as an assessment of the effects on biocompatibility.

EXPERIMENTAL METHODS AND TECHNIQUES

3-mm.-diameter Ni-50.8at.%Ti wire was annealed at 1000°C for 30 min., centerless ground to remove the resultant oxide scale, and electropolished. The wire was subsequently oxidized in an air furnace at 400–1000°C in 100°C increments for 3, 10, 30, 100, and 300 min. Auger Electron Spectroscopy (AES), Focused Ion Beam (FIB), JEOL JSM-5600 Scanning Electron Microscope (SEM), and Oxford Instruments Model 6587 Energy Dispersive X-Ray Spectroscopy (EDXS) were used to characterize the thickness and composition of the oxide layer(s). AES was used for oxide layers up to 0.1 μm, FIB between 0.1–1 μm, and SEM for 1 μm layers. Cross-sections of the wires were prepared using standard metallographic techniques. Two sections of wire from each heat-treatment condition were mounted in bakelite, polished to a mirrorlike finish with 60–1200 grit SiC paper, and cleaned in ultrasonicated denatured alcohol. Samples were not etched in order to ensure that all phases were retained for analysis.

Specimens were observed by SEM in both Secondary Electron Imaging (SEI) and Backscattered Electron Imaging (BEI) modes; the BEI mode was especially useful to differentiate Ni-rich (light) and Ti-rich (dark) phases. Layer-thickness measurements from AES were based on estimates from the FWHM depth profiles, whereas thicknesses from FIB and SEM were based on averages of measurements from several samples.

RESULTS AND DISCUSSION

Oxidation Growth and Composition

No visible oxide was observed by SEM for samples at lower temperatures ($\leq 600^\circ\text{C}$) and at 700°C for shorter times (≤ 30 min.). These samples were analyzed with AES and/or FIB to determine the oxide thickness and composition. Figure 1 shows the AES depth profile of the electropolished and 400°C/3 min. samples, with a TiO₂ thickness of 110 Å and 200 Å, respectively. After 30 min. at 400°C, AES revealed a nickel-rich region beneath the outer TiO₂ layer (Figure 2). The remaining samples analyzed with AES showed a more pronounced nickel-rich region below the TiO₂ layer. Table 1 summarizes the oxide thicknesses as a function of temperature and time; the analytical technique used is also indicated

FIB [12] was used to analyze intermediate oxide thicknesses, as well as to overlap other analysis techniques. Figure 3 shows two light gray superficial platinum layers (marked) that are used as a protective coating during sample preparation. Beneath those layers, a darker TiO₂ (or other Ti suboxide layers) with a lighter nickel-rich sublayer is detected. Chuprina [7] also discovered a “white layer” beneath the surface scale by optical metallography, which he determined to be Ni₃Ti. Voids in the surface layers are also seen in Figure 3. The formation of voids and/or pores may be due to stress generation in the oxide during growth or by the Kirkendall effect whereby vacancies are created when the Ti atoms diffuse away from the NiTi matrix to react with O₂ [7,13–15]. Chu *et al.* [14] suggest that the formation of large voids may be due to the difference in the vertical and lateral oxide growth rates, as well as the collection of vacancies..

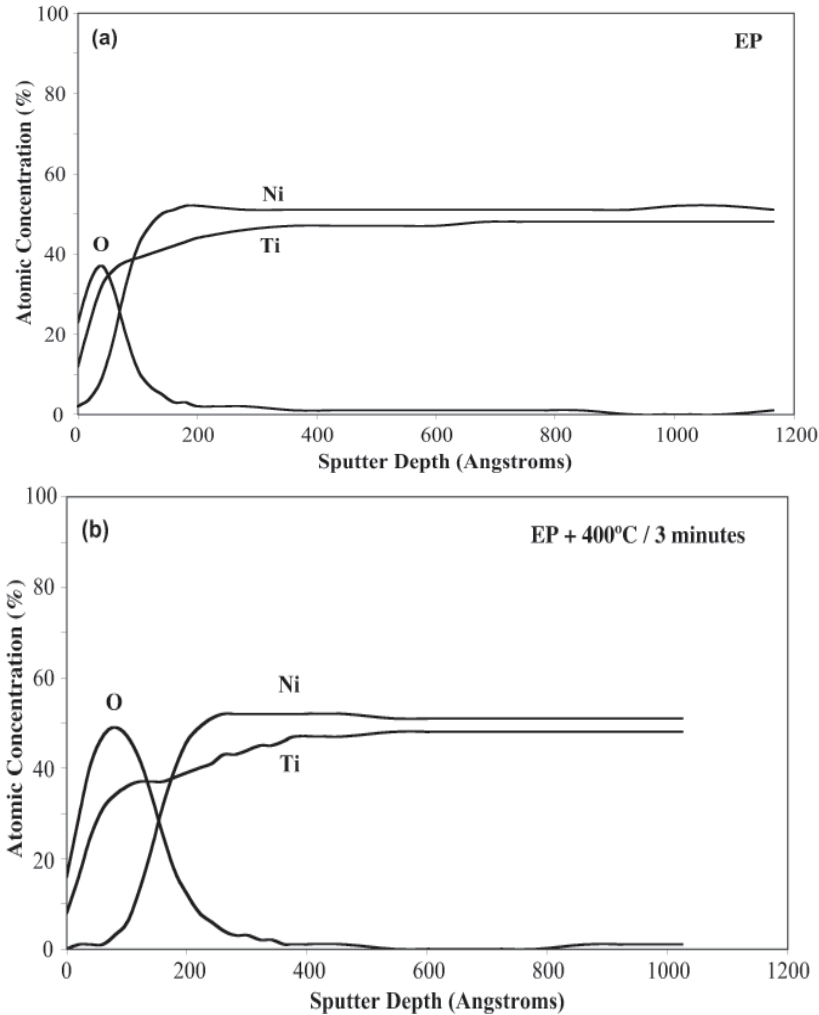


Figure 1 AES depth profiles of NiTi wire: (a) as electropolished; (b) 400°C for 3 min.

Figure 4 shows the cross-section of the as-electropolished wire, as compared to Figure 5, which illustrates the progressive growth of the oxide with increasing time at 900°C. The bright interfacial region between the base NiTi and the surface TiO₂ observed for the oxidized samples was analyzed by EDXS to be 75at.%Ni and 25at.%Ti, consistent with Ni₃Ti (white sublayer); EDXS also confirms the presence of TiO₂ (dark gray). Small Ni₃Ti fingerlike projections emerge from the nickel-rich layer and appear to form islands in the oxide. A comprehensive EDXS analysis indicates that the Ni content of the phases increases with increasing distance from the NiTi interface. The Ni₃Ti interfacial layer transforms to Ni₄Ti (80at.%Ni), whereas the islands become nearly pure Ni (approximately 92at.%Ni). This composition transition indicates that with increasing time at temperature, the Ni₃Ti sublayer becomes Ti-depleted as the Ti reacts with the O₂, leaving behind nearly pure Ni. The light gray areas embedded in the TiO₂ observed in Figure 5e may be NiO and TiO₂, which can react to form the double-oxide NiTiO₃ [16]. Other authors [7–9, 13–14] obtained similar results,

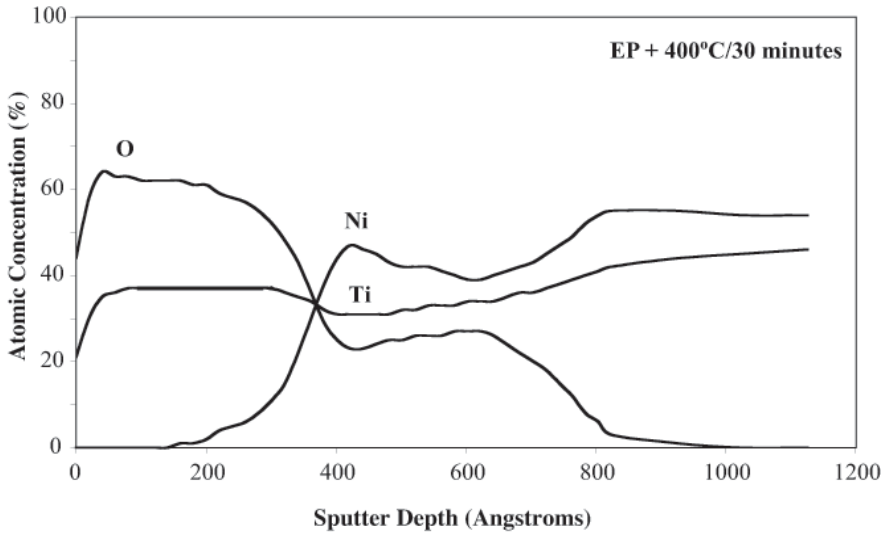


Figure 2 AES depth profile of 400° C/30 min. NiTi wire. Note the presence of a Ni-rich region below the TiO₂ surface layer.

Table 1 Oxide Thickness as a Function of Temperature and Time with Analytical Technique

Time (min.)	Temperature (°C)						
	400	500	600	700	800	900	1000
	Oxide Thickness (μm)						
0	0.0110 A	0.0110 A	0.0110 A	0.0110 A	0.0110 A	0.0110 A	0.0110 A
3	0.0200 A	0.0188 A	0.0338 A	0.180 A	2.737 S	6.052 S	11.23 S
10	0.0338 A	0.0244 A	0.0808 F	0.550 F	5.775 S	11.40 S	21.90 S
30	0.0282 A	0.0676 F	0.534 F	0.738 S	13.70 S	14.70 S	54.80 S
100	0.0470 F	0.0708 F	1.356 F	2.230 S	15.33 S	23.50 S	157 S
300	0.0670 F	0.0714 S	2.650 S	6.780 S	20.92 S	43.80 S	278 S

*Primary Analytical Technique: A = AES, F = FIB, and S = SEM

but there are discrepancies in the actual composition of these phases. X-ray diffraction analysis in Chuprina *et al.* showed the coexistence of Ni₃Ti, Ni, NiO, Ni(Ti), and TiO₂ at high temperatures (>600° C) [7]. Metallic Ni, oxidized Ni, or Ti atoms in solid solution with Ni (Ni(Ti)) have also been reported [9, 13–14].

After 3 min. at 1000° C, the nickel-rich and titanium oxide regions can be observed easily by BEI/SEM (see Figure 6a). The nickel-rich precipitates and TiO₂ form a lamellar structure of alternating Ni-rich phases and TiO₂. After 30 min. at 1000° C, this structure becomes more apparent (see Figure 6b), and after 300 min. at 1000° C, the oxide has become extremely thick (approximately 300 μm), with most of the Ni from Ni₃Ti dispersing into the TiO₂ layer (see Figure 6c). As Ni dif-

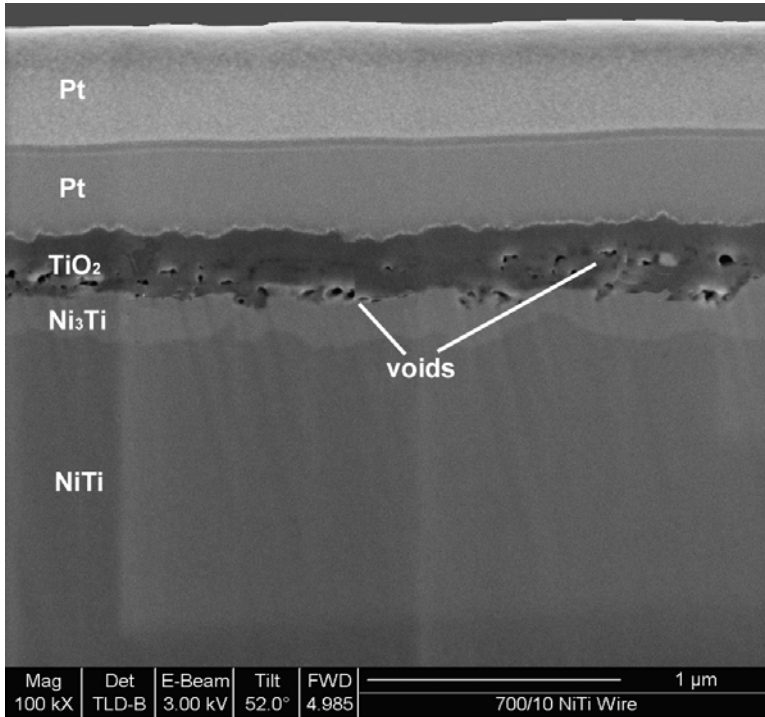


Figure 3 FIB image of 700°C/10 min. NiTi at 100,000 \times . Note the bright Ni₃Ti layer and (dark) voids.

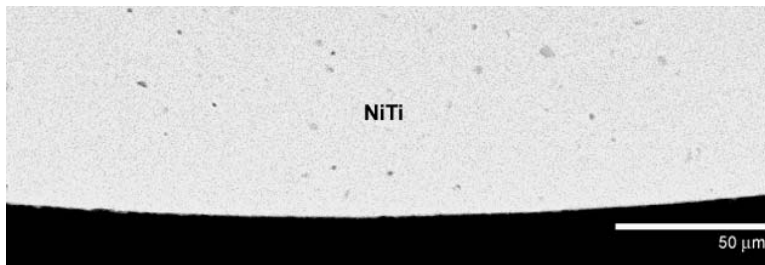


Figure 4 BEI/SEM image of as-electropolished cross-section (500 \times).

fuses to the surface, it becomes increasingly pure (approximately 98at.%Ni), with most of the Ti reacting with O₂ to form TiO₂.

It appears that the TiO₂ layer acts as a diffusion barrier to prevent Ni from oxidizing as expected from pure metal thermodynamics [17]. This is also consistent with the thermodynamic calculations from Firstov *et al.* [13], which indicate that reactions at the NiTi/air interface consist of NiTiO₃, TiO₂, and metallic Ni, whereas NiO would not be formed due to insufficient oxygen partial pressures. Oxidation Kinetics.

Figure 7 illustrates the effect of time and temperature on oxide thickness from the present experimental study. Note that there is an initial high growth rate followed by slower growth kinetics at all temperatures. These data also demonstrate the expected trend of higher oxidation rates at higher

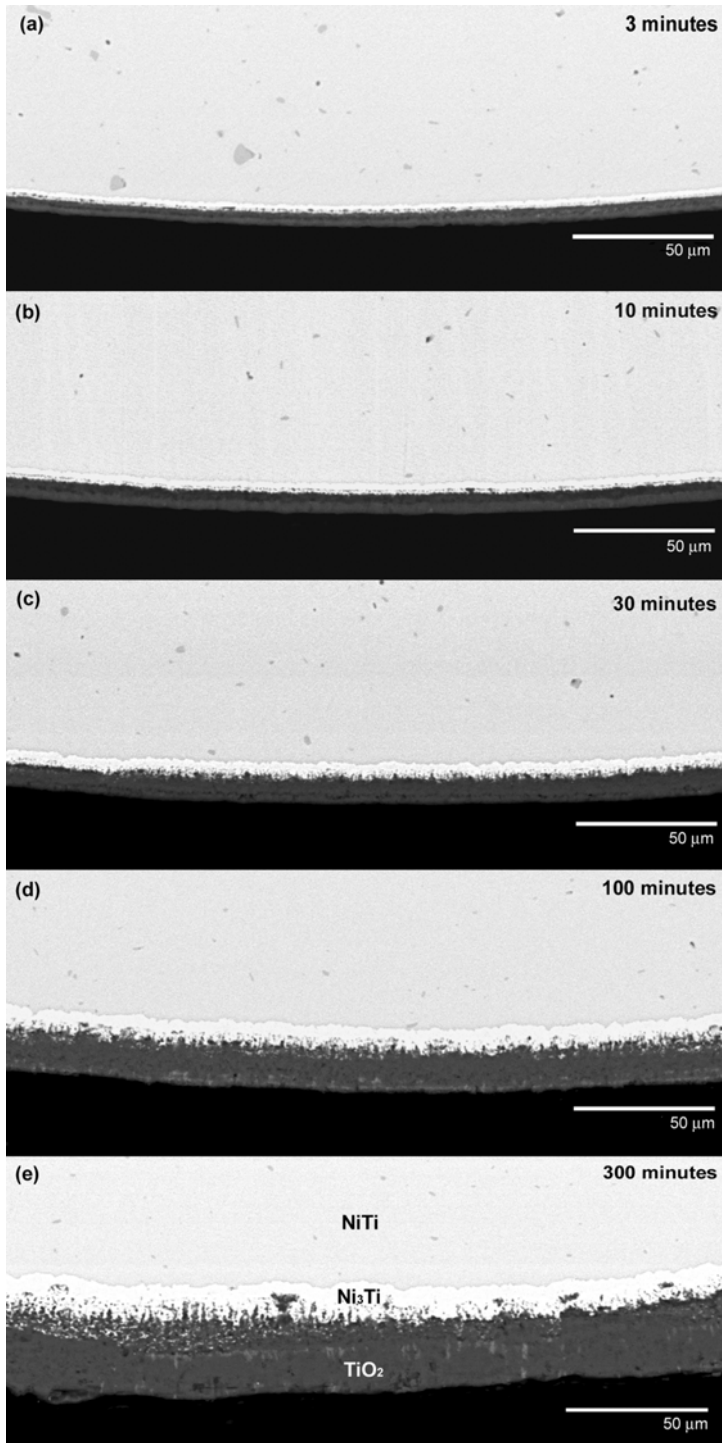


Figure 5 BEI/SEM images of NiTi wire cross-section after 900°C: (a) 3 min. (b) 10 min. (c) 30 min. (d) 100 min. (e) 300 min. (500×).

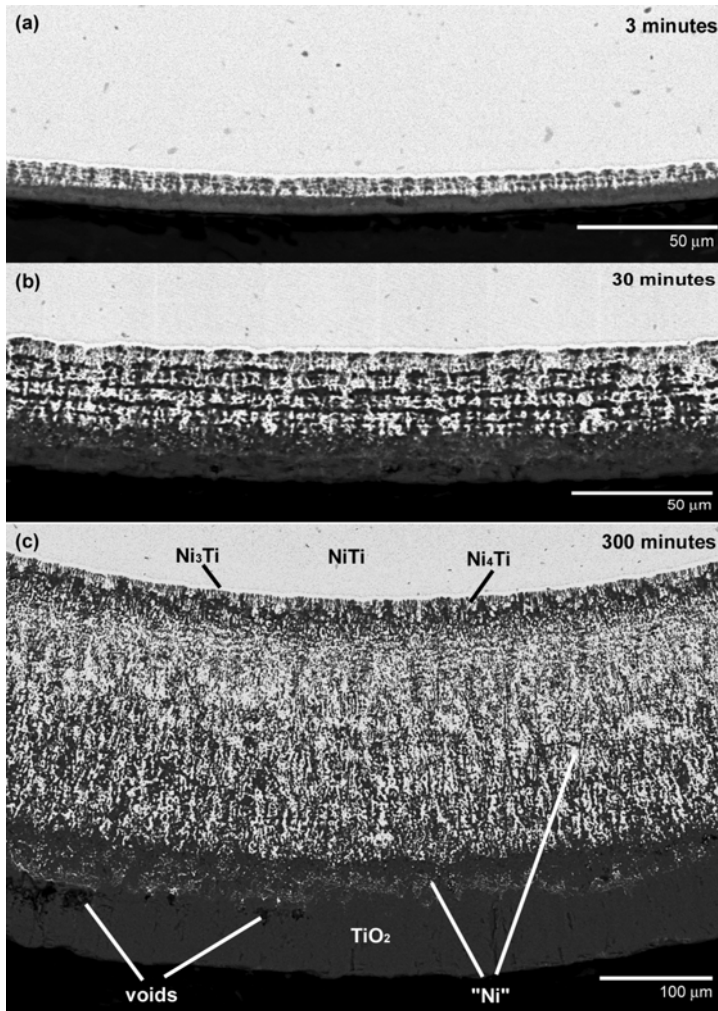


Figure 6 BEI/SEM image of NiTi wire cross-section after electropolishing and a heat treatment at 1000°C : (a) 3 min. ($500\times$), (b) 30 min. ($500\times$), (c) 300 min. ($200\times$).

temperatures. These observations are consistent with a model of oxygen absorption on the NiTi surface that reacts with outward diffusing Ti to form TiO_2 . Chu *et al.* [14] and Keng *et al.* [16] discussed the relative direction of atomic diffusion and phase formation. During the early stages of oxidation, the growth of the TiO_2 layer is the only contributor to thickness and therefore oxide formation is relatively rapid. However, the preferential oxidation of Ti creates a Ti-depleted (Ni-rich) zone at the NiTi/ TiO_2 interface as illustrated in Figures 3–6. The formation of the Ni-rich layer increases the effective diffusion distance with an associated decrease in overall oxidation kinetics. Continued oxide growth therefore involves simultaneous nucleation and growth of titanium oxides and Ni-rich phases. Ultimately, these processes lead to the formation of a protective oxide scale, which prevents further oxidation of the base material. Several authors observed parabolic oxidation rates in NiTi alloys [13–14, 16, 18]. The governing equation can be written as

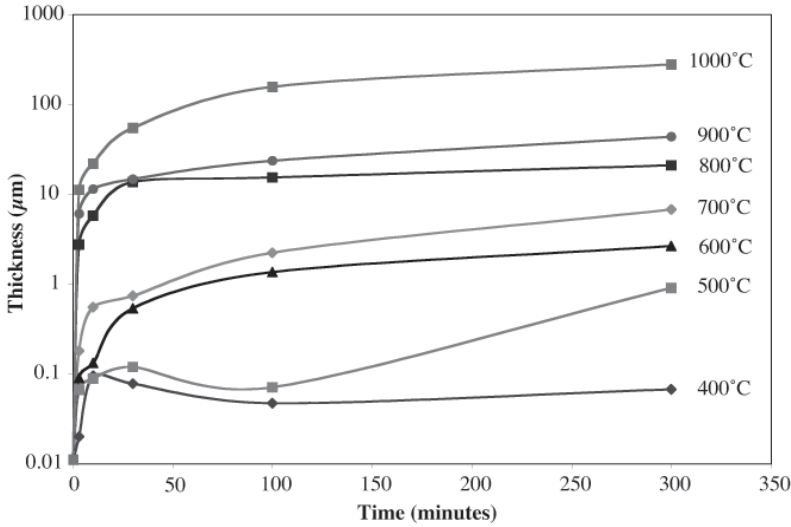


Figure 7 The effect of time on oxide thickness is consistent with parabolic oxide growth.

$$thk^2 = k_p t \quad (1)$$

which indicates that square of the oxide thickness (thk^2) is proportional to time, t , through the parabolic oxidation rate, k_p . Oxidation rates were determined from the data shown in Figure 7. For illustrative purposes, these data were plotted on a log scale. These data can also be modeled with an Arrhenius equation, shown as equation 2, which governs the reaction rates.

$$k_p = k_0 \exp(-Q/RT) \quad (2)$$

where k_0 is the rate constant, Q is the activation energy, R is the gas law constant, and T is the absolute temperature. Figure 8 plots the rate constant as a function of $1/T$ for the seven data sets. An activation energy of 50 kcal/mol was determined from the slope of the curve. This oxidation activation energy is the same order of magnitude as the activation energy to form NiO from pure Ni (45 kcal) and TiO₂ from pure Ti (26 kcal) [19]; these curves are also shown in Figure 8 for comparison. Chu *et al.* [14] obtained an activation energy of 54 kcal/mol (700–1000° C), which agrees well with the present findings. Chuprina *et al.* [7] found a range of activation energies for various heat-treatment temperatures with a transition from low-temperature (600–700° C) oxidation (43 kcal/mol) to high-temperature (700–1000° C) oxidation (72 kcal/mol), which are also consistent with the present data.

Corrosion

The corrosion behavior of these oxidized wires was investigated in a companion study [20]. It was shown that the corrosion resistance is a strong function of oxide thickness where samples with the thinner (<0.1 μm), more pure oxides have higher corrosion resistance. It is further illustrated that the Ni-rich regions in the thicker, less pure oxides promote localized corrosion (pitting).

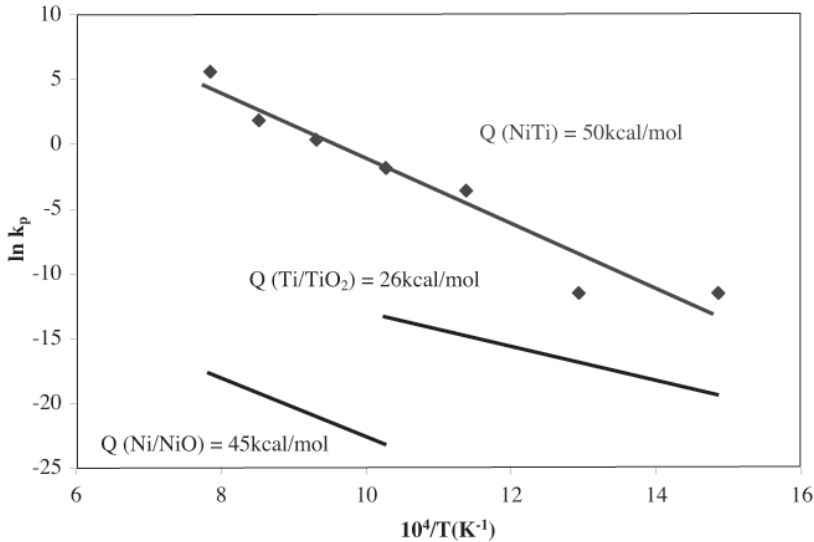
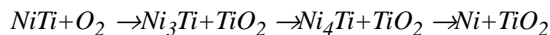


Figure 8 Arrhenius comparison of the oxidation rates for NiTi and Ti in TiO₂ and Ni in NiO [19].

CONCLUSIONS

The present paper shows the phase formation and kinetics of transformations for oxidized NiTi. Electropolished wires are characterized by a thin (~0.01 μm) TiO₂ layer. The thickness of the oxide layer increases with increasing oxidation time at temperature between 400°C and 1000°C. A Ni-rich layer is observed at the interface between NiTi and the thermal TiO₂. Above 800°C the Ni₃Ti interfacial layer transforms into Ni₄Ti with fingerlike projections (approximately 80at.%Ni) and Ni islands (approximately 98at.%Ni) surrounded by TiO₂. The oxidation reactions for these samples appear to proceed as follows:



This oxide growth was determined to be parabolic, with a resultant activation energy of 50 kcal/mol. The parabolic nature of this oxide prevents further high-rate oxidation. The corrosion behavior of NiTi is highly dependent on the thickness and composition of these oxide layers.

REFERENCES

1. T. Duerig, A.R. Pelton, and D. Stoeckel, *Mater Sci Eng* **A273-275** (1999), p. 149–160.
2. D. Stoeckel, *Min. Invas. Ther. & Allied Technol.* **9** (2) (2000), p. 81–88.
3. D.E. Hodgson, M.H. Wu, and R.J. Biermann, in *ASM Metals Handbook ASM*, 10th Ed., Vol. 2 (1991), p. 897–902.
4. J. Ryhanen, in *Min. Invas. Ther. & Allied Technol.* **9** (2) (2000), p. 99–106.
5. C. Trepanier, R. Venugopalan, and A.R. Pelton, in *Shape Memory Implants*, ed. L. Yahia (2000), p. 35–45.

6. R. Venugopalan, and C. Trepanier, *Min. Invas. Ther. & Allied Technol.* **9** (2) (2000), p. 67–74.
7. V.G. Chuprina, *Soviet Powder Metallurgy and Metal Ceramics* **28** (4) (1989), p. 468–472.
8. J.P. Espinos, A. Fernandez, and A.R. Gonzalez-Elipse, *Surf. Sci.* **295** (1993), p. 402–410.
9. R.G. Vichev *et al.*, *Proceedings of the Seventh European Conference on Applications of Surface and Interface Analysis*, eds. I. Olefjord, L. Nyborg, and D. Briggs (Goteborg) (1997), p. 679–682.
10. C. Trepanier *et al.*, *J. Biomed. Mater. Res. (Appl. Biomater.)* **43** (1998), p. 433–440.
11. S. Trigwell *et al.*, *Sufr. Interface. Anal.* **26** (1998), p. 483–489.
12. B.L. Pelton and J. Vitarelli, in *SMST-2000: Proceedings from the International Conference on Shape Memory and Superelastic Technologies*, eds. S.M Russell and A.R. Pelton (Pacific Grove, Calif.: International Organization on SMST), p. 97–102.
13. G.S. Firstov *et al.*, *Biomaterials* **22** (2002), p. 4863–4871.
14. C.L. Chu, S.K. Wu, and Y.C. Yen, *Materials Science and Engineering* **A216** (1996), p. 193–200.
15. A.S. Khanna, *High Temperature Oxidation and Corrosion* (ASM International, 2002).
16. C.L. Zeng, *Oxidation of Metals* **58**, no.1–2 (2002), p. 171–184.
17. D.R. Gaskell, *Introduction to Metallurgical Thermodynamics*, 2nd Ed. (1981), p. 287.
18. V.G. Chuprina, *Soviet Powder Metallurgy and Metal Ceramics* **28**, no. 4 (1989), p. 310–314.
19. O. Kubaschewski and B.E. Hopkins, *Oxidation of Metals and Alloys*, 2nd Ed. (1962).
20. C. Trepanier *et al.* in *SMST-2003: Proceedings of the International Conference on Shape Memory and Superelastic Technologies*, eds. A.R. Pelton and T. Duerig (Pacific Grove, Calif.: SMST Society), these proceedings.