

Effect of Tensile and Compressive Pre-Strains on Superelastic Diamond Surrogates

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Tension – Tension (0<R<1 ; $\varepsilon_M \neq 0$)

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Shamimi et al., SMST 2015

2 2017 Confluent Medical Technologie: Rotary Bend Fatigue (R= -1 ; $\varepsilon_M = 0$)

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N_f [cycles]

Schaffer, J.E., "Mechanical Conditioning of Superelastic Nitinol Wire for Improved Fatigue Resistance", Journal of ASTM International, Vol. 7, No. 5

Rotary Bend Fatigue (R= -1 ; $\varepsilon_M = 0$)

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Number of Cycles to Failure (Nf)

Shamimi et al., Unpublished Data

4



Determine whether residual stresses are the primary mechanism for durability improvement in Nitinol



Origins of Residual Stresses

- Localized yielding from a surface notch or from a multiaxial stress state (Bending, Torsion etc.)
- Microstructural inhomgeneities (Presence of inclusions)
- Grain orientation in a poly-crystalline material

Outline

Computational Modeling of Residual Stresses under

- Bending load (diamond specimens)
- Presence of inclusions (tension specimens)

Test Results of Pre-strain Diamond Study

- Test Methodology
- Baseline without pre-strain on diamonds
- Effect of tensile pre-strain on fatigue life
- Effect of compressive pre-strain on fatigue life

Role of superelasticity in residual stresses



Modeling Residual Stresses Diamond Specimens Tension Specimens Pre-strain Diamond Test Results Role of Superelasticity in Residual Stresses



Pre-Strain Diamond Geometry

Diamonds were designed to achieve high pre-strains.

Only the extrados location of the diamond was focused to achieve the desired stress/strain state.



Stress Free Diamond





ODB: NDC-53-07600-R2-precompress-9%-01.odb Abaqus/Standard 3DEXPERIENCE R2016x HotFix 4 Tue Jan 17 17:21:19 Pacific Standard Time 20:

Step: compress Increment 0: Step Time = 0.000 Primary Var: S, Max. Principal (Abs) Deformed Var: U Deformation Scale Factor: +1.000e+00



Tensile Pre-Stress State



Step: compress Increment 33: Step Time = 1.000 Primary Var: S, Max. Principal (Abs) Deformed Var: U Deformation Scale Factor: +1.000e+00



Compressive Residual Stress State



Compressive Residual Stress – FEA Sequence



Compressive Residual Stress – Test Sequence



Compressive Cyclic Stress – FEA Sequence



Compressive Cyclic Stress – Test Sequence



Modeling Residual Stresses Diamond Specimens Tension Specimens Pre-strain Diamond Test Results Role of Superelasticity in Residual Stresses



Tension Inclusion FEA





Inclusion Size : $4\mu m \times 4\mu m \times 4\mu m$ Mesh Size : $1\mu m \times 1\mu m \times 1\mu m$ Wire diameter : 0.22 mm

Starting State



Void

Inclusion Attached



Stress State – Initial





Void 0 MPa

Inclusion Attached 0 MPa

Stress State – Pull 10% Global Strain





Void 1567 MPa; SIF= 1.27

Inclusion Attached 1757 MPa ; SIF= 1.41

Stress State – Released







Step: release 1-10% Increment 188: Step Time = 1.000 Primary Var: S, Max. Principal (Abs) Deformed Var: U Deformation Scale Factor: +1.000e+00

Void -720 MPa

Inclusion Attached -710 MPa

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2017 Confluent Medical Technologie

Effect of Residual Stresses on Upper Plateau Stress – Without Pre-straining (6% global strain)





Void 1063 MPa

Inclusion Attached 790 MPa



Effect of Residual Stresses on Upper Plateau Stress – With 10% Pre-straining (6% global strain)





Void 741 MPa 30% drop

Inclusion Attached 613 MPa 22% drop

Modeling Residual Stresses Pre-strain Diamond Test Results

Test Methodology

Baseline

Tensile Pre-strain

Compressive Pre-strain

Role of Superelasticity in Residual Stresses



Extrados Stress States – Naming Convention

Pre-Stress/Strain – PS

Residual Stress/Strain – RS (Depends on Pre-Stress history)

Cyclic Stress/Strain – CS

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Combination	<u>Pre-Stress</u> State (PS)	Residual Stress State (RS)	<u>Cyclic Stress</u> State (CS)			
Α	(+)	(-)	(-)			
В	(-)	(+)	(-)			
С	(+)	(-)	(+)			
D	(-)	(+)	(+)			
Inverse Sign						

(+) Tensile(-) Compressive

Hypotheses

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Fatigue life improves when pre-stress and cyclic stress are of same polarity.

Combination	<u>Pre-Stress</u> State (PS)	Residual Stress State (RS)	<u>Cyclic Stress</u> State (CS)			
Α	(+)	(-)	(-)			
В	(-)	(+)	(-)			
С	(+)	(-)	(+)			
D	(-)	(+)	(+)			
Inverse Sign						

(+) Tensile(-) Compressive

Global Force Displacement – Test



Pre-Stress Diamond Test Conditions

Material: SE508-ELI Sample size: 6 Diamonds (or 12 'V' s at each condition) Test Temperature: 37°C

Pre-strain (Tensile or compressive) : 9% Mean strain: 3.50% Starting strain amplitude: 0.75% Run out: 1 million cycles ; Increase cyclic displacements until specimens fracture





Modeling Residual Stresses Pre-strain Diamond Test Results

- **Test Methodology**
- **Baseline**
- **Tensile Pre-strain**
- **Compressive Pre-strain**
- **Role of Superelasticity in Residual Stresses**



Baseline Test Force Displacement



Baseline Test Results

Mean strain: 3.50%

Run out: 1 million cycles

Sample size: 12 at each condition

Strain Amplitude (%)	Baseline (PS0, CS+)	Combination A (PS+, RS-, CS-)	Combination B (PS-, RS+, CS-)	Combination C (PS+, RS-, CS+)	Combination D (PS-, RS+, CS+)
0.75	Run Out				
1.30	Run Out				
1.88	Run Out				
2.24	Fracture (2)				
2.76	Fracture (5)				
2.90	Fracture (3)				
3.03					
3.16					
3.50					

Modeling Residual Stresses Pre-strain Diamond Test Results

- **Test Methodology**
- Baseline

Tensile Pre-strain

Compressive Pre-strain

Role of Superelasticity in Residual Stresses



Global Force Displacement – Test



Tensile Pre-Strain Results

Pre-strain: (+) 9.00%

Mean strain: 3.50%

Run out: 1 million cycles ; Sample size: 12 at each condition

Strain Amplitude (%)	Baseline (PS0, CS+)	Combination A (PS+, RS-, CS-)	Combination B (PS-, RS+, CS-)	Combination C (PS+, RS-, CS+)	Combination D (PS-, RS+, CS+)
0.75	Run Out	Run Out		Run Out	
1.30	Run Out	Fracture (3)		Run Out	
1.88	Run Out	Fracture (4)		Run Out	
2.24	Fracture (2)	Fracture (1)		Run Out	
2.76	Fracture (5)			Fracture (1)	
2.90	Fracture (3)			Fracture (1)	
3.03				Fracture (1)	
3.16				Fracture (3)	
3.50				Fracture (2)	
		Fracture Initiation: Intrados	:	Fracture Initiation: Extrados	

Modeling Residual Stresses Pre-strain Diamond Test Results

- **Test Methodology**
- Baseline
- **Tensile Pre-strain**
- **Compressive Pre-strain**

Role of Superelasticity in Residual Stresses



Global Force Displacement – Test





Compressive Pre-Strain Results

Pre-strain: (-) 9.00%

Mean strain: 3.50%

Run out: 1 million cycles ; Sample size: 12 at each condition

Strain Amplitude (%)	Baseline (PS0, CS+)	Combination A (PS+, RS-, CS-)	Combination B (PS-, RS+, CS-)	Combination C (PS+, RS-, CS+)	Combination D (PS-, RS+, CS+)
0.75	Run Out	Run Out	Run Out	Run Out	Run Out
1.30	Run Out	Fracture (3)	Run Out	Run Out	Fracture (1)
1.88	Run Out	Fracture (4)	Run Out	Run Out	Fracture (3)
2.24	Fracture (2)	Fracture (1)	Run Out	Run Out	Fracture (2)
2.76	Fracture (6)		Fracture (2)	Fracture (1)	
2.90	Fracture (3)		Fracture (4)	Fracture (1)	
3.03			Fracture (4)	Fracture (1)	
3.16				Fracture (3)	
3.50				Fracture (2)	
		Fracture Initiation	Fracture Initiation:	Fracture Initiation: Extrados	Fracture Initiation:

Survival Plot – Diamond Surrogates



Modeling Residual Stresses Pre-strain Diamond Test Results Role of Superelasticity in Residual Stresses



Residual Stress State – Inclusion Attached (Steel vs. Nitinol)



Inclusion Attached

Steel 316L -450 MPa

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Inclusion Attached

Nitinol -710 MPa

Residual Stress State – Void (Steel vs. Nitinol)





Void

Steel 316L -420 MPa

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Void

Nitinol -720 MPa

Summary

Residual stresses through pre-straining can increase or decrease the fatigue life depending on the nature of pre-strain and cyclic stress state.

Fatigue life improves when the pre-stress and cyclic stress are of the same polarity (i.e., tensile or compressive).

The effect of residual stresses is more pronounced in Nitinol compared to a traditional metal.



bit.ly/smst17ndc

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